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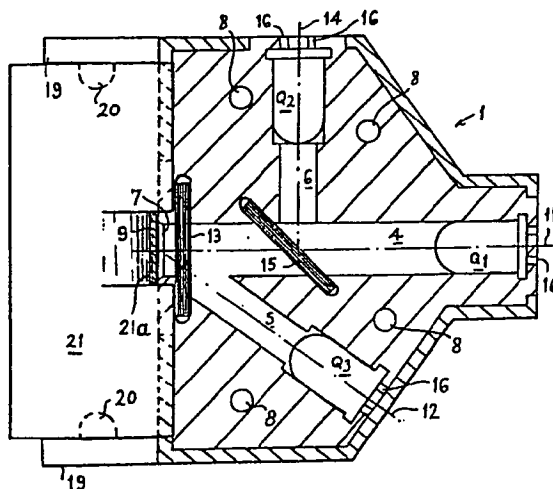
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54 **Reflectometer.**

57 A reflectometer has an optical chamber comprising a light source (Q1) for illuminating a test specimen (9) and a reflectance photosensor (Q3) responsive to light reflected from the test specimen to produce a reflectance signal corresponding to the reflectance of the specimen. The reflectance photosensor (Q3) is disposed along an optical path (5) having its optical axis (12) inclined to the optical axis (11) of the optical path (4) along which light is projected onto the test specimen by the light source (Q1) so that the photosensor (Q3) detects random reflections from the test specimen (9). The optical chamber may also include a reference photosensor (Q2), a beam splitter (15) arranged to reflect a minor fraction of the light emitted by the light source (Q1) onto the reference photosensor, and a drive circuit for the light source which is responsive to a control signal derived from the reference sensor (Q2) and which provides for pulsed operation of the light source so as to maintain the control signal generally at a constant level.



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REFLECTOMETER

1 The present invention relates to reflectometers
and, more particularly, although not exclusively, to
reflectometers used to monitor the colour change of a
test strip in response to its reaction with a fluid
5 specimen applied to the strip. For example, such
reflectometers may be used to monitor the blood/glucose
levels of diabetics by detecting the colour change of a
test strip to which a blood specimen has been applied.
Reflectometers used for this purpose are commonly
10 referred to as "glucometers".

 Ideally, a reflectometer as used, for example, to
measure blood/glucose levels from reactive test strips,
should give consistent reflectance measurements from
standard reflectors regardless of temperature,
15 humidity, or other environmental factors. It should
also produce a consistent measurement for a given
colour standard, regardless of a test strip's surface
shine. Particularly, with dark colours, which absorb
more light, the shine effect produced by directly
20 reflected light does not allow accurate sensing of such
colours.

 Temperature effects on circuits and optical
sensors have proved to be the single largest cause of
reflectance errors and the most difficult of
25 environmental variables to overcome. Hitherto,
relatively low cost reflectometers have endeavoured to
eliminate the temperature effects by having a user
calibrate each time with a dark and light standard
reflector or, at a minimum, with a light standard
30 reflector allowing the dark standard to drift. It has

1 been found that using dark standards contributes very
little to overall accuracy. Since many users reject the
necessity of reflectance calibration every time before
use, many manufacturers have avoided this requirement
5 by assuming that most measurements would be made at
about 25°C ambient. With this arrangement, users are
only required to check reflectance calibration
periodically. However, a check on the performance of
reflectometers presently marketed and having no
10 reference systems, at temperatures of 15°C to 35°C,
shows that such units are subject to errors ranging
from 50% to 100%.

In order for a reflectometer to provide accurate
readings, it is merely necessary for the reflectometer
15 to detect the colour of a specimen or sample and not
the reflected image so that it is unnecessary to detect
directly reflected light, and shine effects can be
alleviated by detecting random or dispersed reflected
light. Accordingly, it is one object of the present
20 invention to provide a reflectometer which detects
random reflections from a test strip or other specimen,
thereby alleviating errors produced by the shine effect
of directly reflected light.

From one aspect, therefore, the invention
25 provides an optical chamber for a reflectometer,
comprising at least one light source arranged to direct
light, along an associated first optical path to
illuminate a test specimen, and at least one
reflectance photosensor disposed along an associated
30 second optical path having its optical axis inclined to
the optical axis of the first optical path and
intersecting the latter at or adjacent the test
specimen, whereby the photosensor detects random

1 reflections from the test specimen. The optical axis of
the second optical path may be inclined at an angle of
at least 20° to the optical axis of the first path and
is, preferably, inclined at an angle of approximately
5 35° .

With this invention, the reflectance sensor is
offset from the optical axis of the first optical path,
along which the light beam from the light source is
projected onto the test specimen, so that whilst the
10 overall amount of light received for a given
reflectance is reduced, it is positioned out of the
shine or halo area and the problem of surface shine,
which may change true reflectance readings, especially
of dark values, by as much as 2%, is reduced or
15 eliminated. By alleviating shine effects, the
reflectance measurement of high absorbing colours is
improved and, in the case of glucometers, for example,
the measurement of higher glucose concentrations, say
in excess of 400 mg/dl, is more accurate.

20 The optical chamber may also include a reference
photosensor associated with the or each light source
and disposed along a third optical path, and means
arranged to reflect a minor portion of the light
projected by the associated light source along this
25 third optical path and onto the reference sensor whilst
transmitting a major portion of the light so as to
impinge on the test specimen.

Conveniently, the or each light source is a light
emitting diode (LED) and the sensors are photodiodes.

30 In one preferred embodiment of the invention
designed for a glucometer, the reference sensor is
disposed along a third optical path which has its axis
substantially perpendicular to the axis of the first
optical path and a beam splitter is arranged to reflect

1 a minor portion of the light emitted by the associated
light source onto the reference sensor. A holder device
is provided for locating a test strip along the first
optical path with the plane of the strip disposed
5 substantially perpendicular to the first optical axis,
and a protective lens device is disposed across the
first and second optical paths adjacent the position at
which the test strip is located.

When LEDs and other light sources are initially
10 excited with a constant current, the emitted light is a
function of the temperature of the source. Light
sources are generally more efficient when cold and the
amount of light emitted decreases, as they warm up,
until a steady state emission is reached. For example,
15 as the junction of an LED heats up, less light is
emitted for the same constant current. The same effect
also holds true for ambient temperature. As ambient
temperature increases, the efficiency of an LED or
other light source decreases. Hence, less light is
20 emitted for a given current as junction or operating
temperature or ambient temperature increases.

Most glucometers solve the temperature problems
of LEDs or other light sources by switching them on for
a relatively long period, say, 30 to 60 seconds, before
25 a measurement is made, thereby allowing them thermally
to equilibrate. This requirement obviously causes the
glucometers to consume unnecessary battery power for
each measurement and thus battery life is reduced.

Accordingly, it is another object of the present
30 invention to avoid the requirement for switching on the
light source of a reflectometer for a long period
before a measurement can be taken. Other objects are to
alleviate errors caused by environmental conditions and
eliminate the need to calibrate for reflectance.

1 From another aspect, therefore, the invention
provides a reflectometer comprising at least one light
source arranged to illuminate a test specimen, at least
one reflectance sensor responsive to light reflected
5 from a test specimen to produce a reflectance signal
corresponding to the reflectance of the specimen, at
least one reference sensor responsive to a fraction of
the light emitted by the light source, and a drive
circuit for the or each light source which is
10 responsive to a control signal derived from the
associated reference sensor and which operates the
light source so as to maintain the control signal
generally at a constant level.

Conveniently, the drive circuit for the light
15 source comprises comparator means which compares the
control signal derived from the reference sensor with a
reference signal and operates the light source so as to
maintain the control signal generally at a constant
level, for example, the level of the reference signal.

20 Hence, with this invention, instead of applying a
constant current to a light source, the light source
may be forced to output the same voltage level
regardless of ambient temperature or the temperature of
the light source. This is achieved by successively
25 switching the light source on and off to produce pulsed
operation with a frequency and pulse width sufficient
to keep the signals derived from the reference sensor
at or in the region of a predetermined constant level
independently of temperature, light source efficiency
30 or reference sensor sensitivity. Consequently, the
light source need only be switched on for a short
period, for example, 1-2 seconds, to permit the
reflectometer to produce a measurement of reflectance.

Preferably, the reflectometer includes means for

1 producing a digital reflectance signal corresponding to
a reflectance sensor output. Such means may include an
analog-to-digital (A/D) converter circuit which
compares an analog reflectance signal derived from the
5 reflectance sensor output with the aforementioned
reference signal and produces a pulse train having a
pulse rate or frequency corresponding to the analog
reflectance signal. This resulting pulse or digital
signal may readily be processed by a central processing
10 unit, such as a microprocessor, to produce a
measurement of the reflectance.

The or each reference sensor may be connected to
amplifying means having an integrating circuit for
integrating the output of the amplifier, and the
15 control signal for the light source drive circuit may
be derived from this amplifier output signal.
Similarly, the or each reflectance sensor may be
connected to amplifying means having an integrating
circuit coupled to its output, and the reflectance
20 amplifier output signal may be processed to produce the
digital reflectance signal.

The output of the reference sensor amplifier may
be connected to a voltage divider circuit for supplying
an adjustable control signal to the light source drive
25 circuit. The output of the reflectance sensor amplifier
may be supplied to the A/D converter network via a
fixed gain amplifier having one input connected to the
reflectance amplifier output and another input
connected to the voltage divider circuit associated
30 with the reference sensor amplifier. The connection of
the drive circuit to the voltage divider may be
adjustable so as to set the light standard reflectance
whilst the connection of the fixed gain amplifier to
the divider may be used to adjust the dark standard

1 reference.

In order that the present invention may be more readily understood, reference will now be made to the accompanying drawings, in which:-

5 Figure 1 illustrates the optical chamber and associated test strip holder of a glucometer embodying the invention, the optical chamber being shown in section taken along the line I-I of Figure 3,

Figures 2 and 3 are, respectively, end and side elevations of the optical chamber illustrated in Figure 1, with the test strip holder removed,

10 Figure 4 illustrates the electronic circuitry of the glucometer,

Figures 5 to 10 illustrate the waveforms of the signals appearing at various terminals of the light source drive circuit and A/D circuit,

15 Figure 11 is a block circuit diagram of the data logger incorporated in the glucometer circuitry, and

Figures 12 and 13 respectively illustrate a plan view and a half section of a modified form of optical chamber.

20 Referring to Figures 1, 2 and 3 of the drawings, the optical chamber of the glucometer comprises a body 1 formed from two parts 2,3 joined together by screws (not shown) engaging in holes 8 in the two parts. The body is preferably made of aluminium, the external surfaces of which have a dull-black anodised finish. Formed within the body are three passageways 4,5 and 6 constituting optical paths or guides. The first optical guide 4 is open at one end 7 and at its opposite end mounts a light source in the form of an LED Q1. The latter is arranged to project light along the first

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1 guide onto a test strip 9 positioned at the open end of
the guide by means of a test strip holder 21. The
second guide 5 intersects the first guide adjacent the
open end 7 of the latter and has a photodiode sensor Q3
5 for sensing reflectance mounted at its end remote from
the first guide. The optical axis 12 of the second
guide intersects the axis 11 of the first guide at the
plane of the open end of the latter and is inclined at
an angle of 35° with respect of the first optical axis
10 11. A protective lens 13, for example, made from glass,
is suitably located across the first and second optical
guides adjacent the open end 7 of the first guide. The
third optical guide 6 has its optical axis 14 disposed
at right angles to the axis 11 of the first guide and
15 intersects the latter at an intermediate position. A
beam splitting lens 15, which may be formed from
plastics material, is disposed in an inclined position
across the first optical guide 4 with its surface
adjacent the LED Q1 located on the point of
20 intersection of the axes 11, 14 of the first and third
guides. The lens 15 reflects a fraction of the light
projected along the first guide by the LED Q1, into the
third optical guide 6 and onto a photodiode reference
sensor Q2 mounted in the third guide, at its end remote
25 from the first guide. The LED and photodiodes Q1, Q2, Q3
are connected in the glucometer circuit by leads
extending through holes 16 in the body 1 behind these
components.

The body 1 has a head 17 at its end adjacent the
30 open end 7 of the first optical guide 4 and a
supporting leg 18 at its opposite end and, in use, it
is stood on a suitable surface in the position shown in
Figure 3. At its head end, the body has spaced opposed
guide walls 19 having vertical guide ribs 20 on their

inner surfaces. The holder 21 for supporting a test strip 9 in position at the open end 7 of the first optical guide 4 is in the form of a plug and is attached to the body by sliding it in between the guide walls 19, in engagement with the guide ribs 20. The holder is arranged to locate a test strip, which is slid into a slot 21a between the holder and optical chamber, across the open end of the first optical guide and press it into contact with the latter.

The LED Q1 is preferably an infra-red LED emitting light in the region of 940 nm wavelength. The light emitted by Q1 travels down the first optical guide 4 and strikes the lens 15 which may, for example, be a .040 inch (approx. 10 mm) thick acrylic sheet. This lens is arranged to transmit 96% of the light projected by Q1 and to reflect 4% of this light onto the photodiode Q2. The optical guides 4,5,6 may be blackened with infra-red absorbing paint to eliminate most light coming at an angle of 10° or more thereby to force most of the incident light impinging on a test strip 9 to be as close as possible to 90°. Some light incident on the test strip is absorbed relative to colour and the remainder is reflected back into the optical guide 4 at various angles, depending on the surface of the strip and the pressure applied to the back of the strip by the strip holder 21. Most of the light is reflected back at an angle of 14° or less and is highly subject to the shine of the strip surface. However, the photodiode reflectance sensor Q3 is offset from the optical axis of the first guide 4 by 35° so that it is positioned out of the shine or halo area. By eliminating these shine effects, measurement of high absorbing colours is improved and glucose measurement in excess of 400 mg/dl is more accurate.

1 Since the light incident on photodiode reference
sensor Q2 is independent of the colour of a test strip
and is only a function of the incident light emitted by
the LED Q1, it is used as a reflectance standard, as
5 will hereinafter be more fully described, to give an
output voltage corresponding to 100% reflectance.

The electronic circuit of the glucometer is
illustrated in Figure 4 and basically comprises a
central processing unit, conveniently, a microprocessor
10 U6, such as that marketed by National Semiconductor
Corporation under the Model No. COPS 444, a
crystal-controlled clock circuit 22, a power supply and
battery-run down detector circuit 23, LED drive and
reflectance sensor circuits 24, A/D circuits 25, a
15 visual display unit U10 and associated display driver
circuit U8, a non-volatile memory U7 for calibration
storage, a battery-backed, plug-in data logger 26, and
an alarm circuit 27, all of which circuit elements are
coupled to and controlled by the microprocessor U6.

20 The power supply circuit comprises a battery B,
for example, a 9-volt battery, two transistors Q4,Q5,
current limiting resistors R1,R2, a diode D1, a voltage
regulator 28, a capacitor C2 connected across the
battery and serving as a power supply filter, and
25 manual 'on' and 'off' switches or keys S1,S2. The
transistor Q4 serves to allow the microprocessor U6 to
switch the power on and off in response to actuation of
the keys S1 and S2, whilst Q5 serves as a buffer
between the microprocessor and the switching transistor
30 Q4. The voltage regulator 28 is a 5-volt regulator used
to maintain the glucometer operating voltage within
acceptable limits for the circuits. In this case, the
regulator maintains a relative constant 5-volt power
supply at its output.

1 Amplifier U9B is connected as a battery run-down
detector and in conjunction with resistors R3,R4,R5 and
R6 constantly monitors the input to the voltage
regulator 28. Capacitor C1 serves as a filter. When the
5 voltage input to the regulator 28 falls below 6 volts,
the output of the amplifier U9B goes high, indicating
to the microprocessor U6 that the battery B is weak.
Consequently, the microprocessor stops further
processing and the system is shut down. A battery
10 warning indication may be displayed on the display unit
U10 for a predetermined period, for example, 15
seconds, before the system is shut down.

The drive circuit for the LED Q1 comprises an
amplifier U3B which serves as a comparator and controls
15 switching of a transistor Q6 connected in series with a
current limiting resistor R20, the LED Q1 and an
enabling transistor Q7, between the 5-volt power supply
and ground. The transistor Q7 is controlled by the
microprocessor U6, via a terminal D2 and an MOS
20 transistor U4C. The latter is connected to the base of
transistor Q7, via a current limiting resistor R18, and
between the power supply and ground, via a current
limiting resistor R19. Capacitor C13 serves as an LED
drive filter.

25 A reference voltage is applied to the input
terminal or pin 3 of the comparator amplifier U3B
whilst a switching control signal derived from the
reference sensor Q2 is applied to the other input pin
2. The reference voltage is supplied by a voltage
30 divider consisting of resistors R9 and R10 connected
between the power supply and ground and having the
junction between the resistors connected to the pin 3
of amplifier U3B. This reference voltage is also
applied to the input pin 5 of a reference amplifier U3A

1 connected as a voltage follower. The pin 5 and the
output pin 7 of this amplifier are at the same
approximate voltage. The resistor R21 connected to the
output of the reference amplifier U3A serves only as a
5 load resistor. The voltage signal at the output pin 7
of the reference amplifier serves as a voltage
reference for the A/D converter circuitry as will
hereinafter be more fully described.

The cathode of the reference photodiode sensor Q2
10 is connected to one input pin 2 of a reference sensor
amplifier U2 having its other input pin 3 connected
directly to ground. The output pin 6 of this amplifier
is connected to a voltage divider network comprising
resistors R13, R14, R15 and R16 which serves for
15 calibration purposes. The control signal for the
comparator amplifier U3B is obtained from an adjustable
tap on the resistor R14, and resistor R13 and R14
together adjust the fraction of the voltage output at
the pin 6 of amplifier U2 which is applied to the input
20 pin 2 of amplifier U3B. Capacitor C12 serves as a
filter for the control signal whilst capacitor C14
serves a filter for the amplifier U2 output. Resistor
R12 and capacitor C4 connected in parallel across the
amplifier serve to integrate the amplifier output and
25 reduce noise.

The cathode of the reflectance photodiode sensor
Q3 is connected to one input pin 2 of a reflectance
amplifier U1 having its other input pin 3 connected
directly to ground. Resistor R8 is a load resistor
30 connected to the output pin 6 of the reflectance sensor
amplifier and resistor R7 and capacitor C3 connected in
parallel across the amplifier from an integrating
circuit which integrates the amplifier output and
reduces noise. The pin 6 of the reflectance sensor

1 amplifier is connected to one input pin 10 of a chamber
difference amplifier U3D having its other input pin 9
connected via an amplifier gain resistor R17 to an
adjustable tap on the resistor R16 of the voltage
5 divider network connected to the output of the
reference sensor amplifier U2. The resistor R11 is an
amplifier gain resistor. The amplifier U3D is a fixed
gain amplifier which amplifies the output of the
reflectance sensor amplifier U1 by two times minus the
10 voltage appearing at the adjustable tap of the resistor
R16. The output of the chamber difference amplifier U3D
is an analog signal representing the output of the
reflectance sensor Q3 and is fed to the A/D circuitry
for conversion into a digital signal representing the
15 reflectance sensor output, as will hereinafter be more
fully described.

The LED drive circuitry operates as follows. The
reference voltage, for example, 1.146 volts, produced
by the voltage divider R9, R10 is applied to the pin 3
20 of the comparator amplifier U3B which compares it with
the fraction of the output voltage of the reference
sensor amplifier U2 applied to the pin 2 of the
comparator amplifier. If the voltage appearing at the
pin 2 of amplifier U3B is less than the voltage at pin
25 3, the output voltage at pin 1 of U3B goes high and the
transistor Q6 is switched on, thereby causing more
current to flow through the LED Q1. The increased
output of Q1 causes reference sensor Q2 to increase its
voltage output, thereby causing the output of amplifier
30 U2 to increase. When the voltage at pin 6 of the
amplifier U2 is sufficient to cause the voltage at the
pin 2 of the amplifier U3B to be larger than that at
its pin 3, the output of the amplifier U3B goes low,
turning off the LED Q1. The voltage at output pin 6 of

1 the amplifier U2 then begins to decay because no light
is incident on the reference sensor Q2 and eventually
decreases below a value sufficient to keep the
potential at pin 2 of amplifier U3B above that of the
5 pin 3, whereupon the transistor Q6 is turned on and the
process is repeated (see Figs. 5 and 6). Consequently,
the LED Q1 is continuously pulsed on and off (see Fig.
7) with a frequency and pulse width sufficient to
maintain the mean voltage at the pin 2 of the amplifier
10 U3B at the reference voltage supplied by the voltage
divider R9,R10 irrespective of temperature, LED
efficiency or the sensitivity of reference photodiode
Q2.

The resistor R14 is used to adjust the fraction
15 of the voltage output at pin 6 of the amplifier U2 to
be applied to the pin 2 of the comparator amplifier
U3B. The higher the fraction, the less light is emitted
by the led Q1 to enable control and the less light is
incident on the reflectance sensor Q3 for a given
20 reflector. Normally, a 90% reflector is inserted into
the test chamber and the resistor R14 is adjusted such
that LED Q1 emits sufficient light to cause the output
of the reflectance sensor amplifier U1 to give a
voltage corresponding to a 90% reflectance when 100% is
25 equal to 1.146 volts, the reference voltage. The
resistor R16 is used to adjust the dark reference. For
this purpose, a 4.5% standard reflectance is inserted
into the test chamber and the resistor R16 is adjusted
until the correct voltage appears at the output pin 8
30 of the chamber difference amplifier U3D. All optical
chambers have stray reflectances, including those which
are off the protective lens 13 in front of the test
strip. These are usually greater than that received
from a 4.5% reflector. Consequently, when calibrating

1 the low or dark reflectance reference, the offset
reflectances and the effects of the amplifier's input
offset voltages must be subtracted. The fixed gain
amplifier U3D is used for this purpose.

5 Hence, the resistor R16 is used to subtract
offset errors from the amplifiers and stray
reflectances to enable an accurate low reflectance
reading whilst the resistor R14 is used to calibrate
the high reflectance reading. Since the whole system is
10 a function of the reference voltage applied to the
input pin 5 of the reference amplifier U3A and since
all calibration voltages are derived from the output of
the reference amplifier whose output is a function of
this same reference voltage, the system is truly ratio
15 metric and independent of battery voltage and absolute
readings, as well as environmental conditions. The
system is self-regulatory, requiring very short bursts
of light current to enable a reflectance reading and
thereby prolonging battery life.

20 The A/D converter circuitry 25 basically
comprises a D-type flip-flop U5, an integrating
amplifier U3C and a comparator amplifier U9A. The
output of the reference amplifier U3A serves as a
reference for both the analog system and the converter,
25 thereby enhancing the ratio metric qualities of the
overall system, and is connected to one terminal of two
MOS transistors U4A, U4B, connected in series between
the output pin 7 of U3A and ground and controlled by
the D-type flip-flop U5. The capacitor C6 connected
30 between the output pin 7 and ground serves as a
reference follower filter. The flip-flop U5 is
triggered by signals applied to its input D from the
output of the comparator amplifier U9A.

The reflectance signal appearing at the output

1 pin 8 of the difference amplifier U3D is integrated by
resistor R22 and capacitor C5 connected between the
output pin 8 and ground and is applied to one input pin
12 of the integrator amplifier U3C. The other input pin
5 13 of this amplifier is connected to the junction of
the two transistors U4A,U4B, via a filter resistor R23,
and to the output pin 14 of the amplifier via an output
filter capacitor C12. The output pin 14 of the
integrating amplifier U3C is connected to one input pin
10 5 of the comparator amplifier U9A by a filter resistor
R24 which is also connected to ground by a capacitor C7
and serving as a delay. The other input pin 6 of the
amplifier U9A is connected to a reference voltage
supplied by voltage divider resistors R25,R26 connected
15 between the power supply and ground.

The A/D converter 25 is of the pulse width
modulation type and is controlled by the microprocessor
U6 which is fed with a digital signal via the terminal
G3 connected to the output pin 2 of the flip-flop U5.
20 When the reflectometer is taking a reading, the
reflectance signal appearing at the output pin 8 of the
chamber difference amplifier U3D is integrated by the
resistor R22 and the capacitor C5 and is applied to the
input pin 12 of the integrator amplifier U3C. Assuming
25 that, at time 0, the state of the flip-flop U5 is pin 1
= low and pin 2 = high, then the voltage at the pin 10
of transistor U4A is zero. The voltage appearing at the
pin 12 of amplifier U3C is initially zero, regardless
of the output voltage on pin 8 of amplifier U3D and
charges slowly to the output voltage of amplifier U3D.
30 As the capacitor C5 charges, the voltage applied to pin
12 of amplifier U3C exceeds the potential at pin 13,
whereupon the output potential at pin 14 begins slowly
to climb. When the voltage at pin 14 exceeds the

1 reference voltage developed by the voltage divider
 R25,R26, the output pin 7 of the comparator amplifier
 U9A goes high triggering flip-flop U5 and causing its
 state to change to pin 1 = high, pin 2 = low, thereby
 5 connecting the negative input of amplifier U3C to the
 circuit reference voltage at pin 7 of amplifier U3A.
 Amplifier U3C then commences to discharge until the
 voltage at output pin 14 decays below that at input pin
 6 of comparator amplifier U9A, whereupon the flip-flop
 10 U5 is reset and the cycle repeats (see Figs. 8, 9 and
 10).

The net result of this sequence of operations is
 the production of a digital signal having a frequency
 or pulse rate whose mark space ratio is a function of
 15 the ratio of the reflectance sensor output signal at
 the pin 8 of the amplifier U3D to the reference signal
 at the output pin 7 of the reference amplifier U3A. The
 microprocessor U6 counts the pulses appearing at the
 pin 2 of the flip-flop U5 via terminal G3 and develops
 20 a binary count according to the following formula:-

$$\text{Counts} = \frac{V_{\text{pin 8}}}{V_{\text{pin 7}}} \cdot 4096$$

The microprocessor consequently receives a
 digital count directly related to the ratio of the
 25 reflectance sensor output signal to the reference
 voltage. On detecting a pulse count, the microprocessor
 accesses a look-up table permanently stored in its read
 only memory (ROM) and operates the display driver U8 to
 display a corresponding glucose level on the visual
 30 display unit U10.

The audio alarm 30, which may for example be 2
 kHz piezoelectric disc, is excited by the
 microprocesssor U6 via transistors U4D and Q8. The
 resistor R27 is a current limiting resistor. The alarm

1 tone is emitted each time a key is depressed, for
example , to warn a user when to wipe a test strip 9
and when a reading is complete.

The amplifiers U3A-D may be formed as parts of a
5 single chip component as may also the MOS transistors
U4A-D and the amplifiers U9A and B.

Upon depressing the 'on' key S1, the
microprocessor U6 is initialised and immediately causes
the alarm 30 to issue a short audio tone, for example,
10 for 200 ms, to acknowledge that the 'on' key has been
depressed. Initially, the microprocessor makes the
following checks:-

1. Checks battery B voltage
2. Checks if calibration data is stored in the
15 memory U7
3. Checks if the LED Q1 is functioning.

After these initial checks, the microprocessor
checks to determine whether normal or factory
calibration has been selected. Factory calibration
20 selection is not available to the end user. If factory
calibration is selected (by shorting the pin 5 on the
microprocessor U6 to ground) the microprocessor
initially checks all segments of the display U10 and
external memory locations. The memory U7 is erased when
25 this check is completed thus destroying all previous
calibration data as well as stored glucose values. It
then goes into a continuous reflectance test mode,
whereby the display U10 constantly shows the A/D count
of whatever it sees in the optical chamber. The system
30 must be turned off to exit this mode. This mode is used
to calibrate the glucometer and for long term accuracy
tests.

If normal mode is selected, the microprocessor U6
checks to determine if the free reflectance (no test

1 strip 9 in the chamber) is 37 +/- 1%. If it is below
36%, but greater than 33%, the microprocessor indicates
"CLEN" on the display U10. If it is below 33%, the
microprocessor indicates "ER1" on the display. It then
5 shuts down, indicating that the chamber is too dirty to
get accurate measurements.

Assuming the glucometer passes the chamber clean
test, the microprocessor U6 then checks to determine if
calibration data is stored in the memory U7. If not,
10 the processor displays "CAL" for one second and then
indicates that a time sequence is next. This is the
normal test sequence. It should be noted that the
microprocessor has stored in its ROM the characteristic
curve for glucose concentration versus percent
15 reflectance. The calibration routine is required only
to modify the curve to account for ageing and
lot-to-lot variance. In most cases calibration is not
required. The glucometer actually does not demand it
and will continue to test even if modifying calibration
20 data is not stored in the memory U7. If calibration
data is stored in that memory, the microprocessor does
not display "CAL" but goes directly to "SEC" (time
indication) and awaits the depression of the time key
S3. It then scans only the on/off keys S1, S2 and the
25 time key S3. Upon depressing the time key, when the
user has deposited blood on a test strip 9, the system
immediately acknowledges the key depression by issuing
a short tone on the audio alarm 30 and shows the time
count on the display U10. At 58 seconds the system
30 issues a short "get ready to wipe" audio tone; at 59
seconds another short "get ready to wipe" audio tone is
issued. At 60 seconds a longer 500 ms audio tone is
issued, indicating the strip should be wiped. At 89
seconds an audio tone is issued, indicating that it is

1 too late to insert the strip 9 if this has not already
been done. At 90 seconds the LED Q1 is switched on by
the microprocessor and the A/D converter is taken
through one A/D conversion cycle to charge all A/D
5 capacitors. At 91 seconds another A/D conversion is
detected. On this occasion, the microprocessor U6
retains the count and converts it to a ratio/count
4096. The microprocessor then goes to the look-up
tables to retrieve the corresponding glucose
10 concentration value and checks the memory U7 to
determine if the concentration should be modified. If
there is no external calibration data written in the
memory U7, the microprocessor causes the audible alarm
30 to issue a short tone and displays the concentration
15 on the visual display U10. At the same time, the
reading obtained is written into the memory U7 and into
the data logger 26. The data output to the data logger
26 is in serial fashion with a "1" being 10 clock
pulses long and "0" being 5 clock pulses long. The
20 microprocessor also supplies the data logger with
information as to whether received data is in mg/dl or
mmol/litre.

The memory U7 is used to store the calibration
data and a sequence of fifteen glucose readings. A
25 reading is written into the memory if the calibration
key S4 is depressed and the stored readings are
accessible to the user simply by depressing the recall
key S5. With each depression of the key S5, the
microprocessor displays on U10 the reading stored in
30 the memory U7 in a last in-first out sequence. The data
is automatically stored in the memory U7 each time a
reading is taken by the glucometer.

The glucometer circuit incorporates an automatic
shut-down feature. If no key has been actuated within a

1 period of two minutes from actuation of the 'on' key
S1, the microprocessor automatically turns off the
power to enhance battery life. Automatic shut-down also
occurs if a bad light source Q1 is detected or if the
5 optical chamber is detected to be dirty.

As illustrated in Fig. 11, the data logger 26
comprises a microprocessor 31, for example, an 8-bit
microprocessor such as an MC68L05, a real time clock
32, a RAM 33 and a ROM 34. After the real time clock 32
10 has been set at a doctors office, the logger module is
plugged into the glucometer. Upon insertion, the audio
alarm 30 is actuated to issue a short tone to
acknowledge successful insertion and "STO" (indicating
storage) is briefly displayed on the visual display
15 U10. Thereafter, whenever a reading is taken the
glucometer microprocessor U6 issues a flag to the
logger microprocessor 31 to accept input data. Data is
supplied serially, in the format mentioned above, in
straight binary followed by two parity bits. At this
20 time, the glucometer displays above the glucose reading
"STO" to signify that data is being stored. Upon
successful transfer of glucose data, the logger
microprocessor 31 reads the real time clock 32 and
stores all data in the logger RAM 33. The latter and
25 clock power are supplied from a self-contained battery.
All other elements receive power from the glucometer
power supply circuit 23. The ROM 34 stores the main
logger sequence and logic programme and serves no
function in storage of glucose/ time data. If the
30 module is now unplugged from the glucometer and is
inserted into a printer 35, the microprocessor 31
begins to output data in ASQ1 II in the following
format, last reading first:-

<u>Date</u>	<u>Time</u>	<u>Reading</u>
4/21	3:03 p.m.	120
4/20	4:05 p.m.	* 250
4/19	4:00 p.m.	# 60

5 The "*" and "#" are used to highlight high and low readings respectively.

The logger microprocessor 31 only reads storage cells in the RAM 33 containing data and prints "END" when it reaches an empty cell so as not to print all unused spaces in the RAM. Since the output format is an industry standard and module can be adapted to
10 virtually all 20 or more column printers.

Figures 12 and 13 illustrate another embodiment of optical chamber for a glucometer, which chamber
15 comprises duplicate sets of LEDs Q1, photodiode reference sensors Q2 and photodiode reflectance sensors Q3. Similarly to the first embodiment, it comprises a two-part body 40. The latter has two sets of passageways 41,42 constituting optical paths or guides,
20 the first guide 41 of each set being open at one end 43 and having the LED Q1 at its opposite end, and the second guide 42 having an open end 44 adjacent the open end 43 of the first guide and having the reflectance sensor Q3 at its opposite end. Light from each LED Q1
25 is projected along the associated first guide 41 so as to impinge on a test strip (not shown) supported in a suitable holder (not shown) adjacent the open ends 43 of the guides 41. Each second guide 42 has its optical axis 45 inclined to the optical axis 46 of the associated first guide and intersects the axis of the
30 first guide at a point in front of the open ends of the

1 guides and adjacent the position at which the test
strip is supported. The optical axis 45 of each second
guide is inclined at an angle of approximately 35° to
the axis 46 of the associated first guide.

5 The reference sensors Q2 are mounted in a housing
47 disposed above the first optical guides 41
intermediate the ends thereof. The housing comprises a
cavity 48 communicating with a cavity 49 formed along
the first optical guides 41. The reference sensors Q2
10 are mounted along optical axes 50 parallel to the
optical axes 46 of the first guides and a small
fraction of the light emitted by each LED Q1 is
reflected onto the associated reference sensor Q2 by a
beam splitting lens 51 mounted in an inclined position
15 across the cavity 49 and, hence, relative to the first
optical axes 46, and a reflector 52 mounted in an
inclined position in the cavity 48.

Each set of LED and photodiodes Q1, Q2, Q3 may be
connected in an LED drive and reflectance sensor
20 circuit 24 as described above, utilising a multiplexer
to interconnect this circuitry with the remainder of
the glucometer system so as to produce reflectance
readings from each reflectance sensor Q3.

Whilst particular embodiments have been
25 described, it will be understood that modifications can
be made without departing from the scope of the
invention as defined by the appended claims. For
example, the electronic system may be arranged
automatically to store glucose readings in the memory
30 U7 (15 readings) instead of as at present, requiring
the user to depress a store key S4 to enable storage.
The "CLEN" indicator and initial reflectance check upon
power-on may be eliminated. This function, as presently
programmed, requires the pressure plate pressing up

1 against the back of strip 9 to have a 34% reflectance
(equivalent to 106 mg/dl of glucose). If no strip is in
the strip holder unit, the latter could read 106 mg/dl
giving user a false reading. This feature may be
5 eliminated by making the pressure plate reflectance
less than 20% thus giving a high reading if no strip 9
is in the holder. The "ER1" function may be reduced to
a simple lamp check, as opposed to checking if the
optical chamber is dirty. It is difficult to access a
10 dirty chamber by checking reflectance from the pressure
plate. "ER1" may then be used to indicate a serious
circuit or lamp malfunction. The "CAL" indicator may be
eliminated if the unit does not have modifying CAL
data. The system will still be capable of being
15 calibrated by the user. However, it is believed this
will be unnecessary and thus will keep the function if
it is ever needed. This will depend upon ageing
characteristics of the strip.

CLAIMS

- 1 1. An optical chamber for a reflectometer, comprising
at least one light source (Q1) arranged to illuminate a
test specimen (9) via a first optical path (4,41) and
at least one reflectance photosensor (Q3) for detecting
5 light reflected from said test specimen, characterised
in that the reflectance photosensor (Q3) is disposed
along a second optical path (5,42) having its optical
axis (12,45) inclined to the optical axis (11,46) of
the first optical path (4,41) and intersecting said
10 first optical axis (11,46) at or adjacent the test
specimen (9), whereby the photosensor (Q3) detects
random reflections from the test specimen.
2. An optical chamber according to claim 1,
characterised in that the optical axis (12,45) of the
15 second optical path is inclined to the optical axis
(11,46) of the first optical path at an angle of at
least 20° and, preferably at an angle of approximately
35°.
3. An optical chamber according to claim 1 or 2,
20 characterised in that the test specimen (9) is in the
form of a test strip, and means is provided for
locating said test strip along the first optical path
(4) with the plane of said strip disposed substantially
perpendicular to the first optical axis (11), and
25 further characterised in that a protective lens device
(13) is disposed across the first and second optical
paths (4,5) adjacent the position at which the test
strip (9) is located.
4. An optical chamber according to claim 1, 2 or 3,
30 characterised by at least one reference photosensor
(Q2) disposed along a third optical path (6,48), for
example, having its optical axis (14) substantially

- 1 perpendicular to the optical axis (11) of the first
optical path (4), and beam splitter means (15,51)
arranged to reflect a minor fraction of the light
emitted by said at least one light source (Q1), along
5 the third optical path (6,48) and onto the reference
sensor (Q2) whilst transmitting a major fraction of the
light so as to impinge on the test specimen (9).
5. An optical chamber according to claim 4,
characterised by a drive circuit for the or each light
10 source (Q1) which is responsive to a control signal
derived from the associated reference sensor (Q2) and
which operates the light source to maintain the control
signal at a generally constant level.
6. An optical chamber according to claim 4 or 5,
15 characterised in that the or each light source (Q1) is
a light emitting diode and the sensors (Q2,Q3) are
photodiodes.
7. A reflectometer including an optical chamber having
at least one light source (Q1) for illuminating a test
20 specimen (9), and at least one reflectance photosensor
(Q3) responsive to light reflected from the test
specimen to produce a reflectance signal corresponding
to the reflectance of the specimen, characterised by at
least one reference photosensor (Q2) responsive to a
25 fraction of the light emitted by said at least one
light source (Q1), and a drive circuit (24) for the or
each light source which is responsive to a control
signal derived from the associated reference sensor
(Q2) and which operates the light source (Q1) so as to
30 maintain said control signal generally at a constant
level.
8. A reflectometer according to claim 7, characterised
in that the drive circuit comprises comparator means
(U3B) which compares the control signal derived from

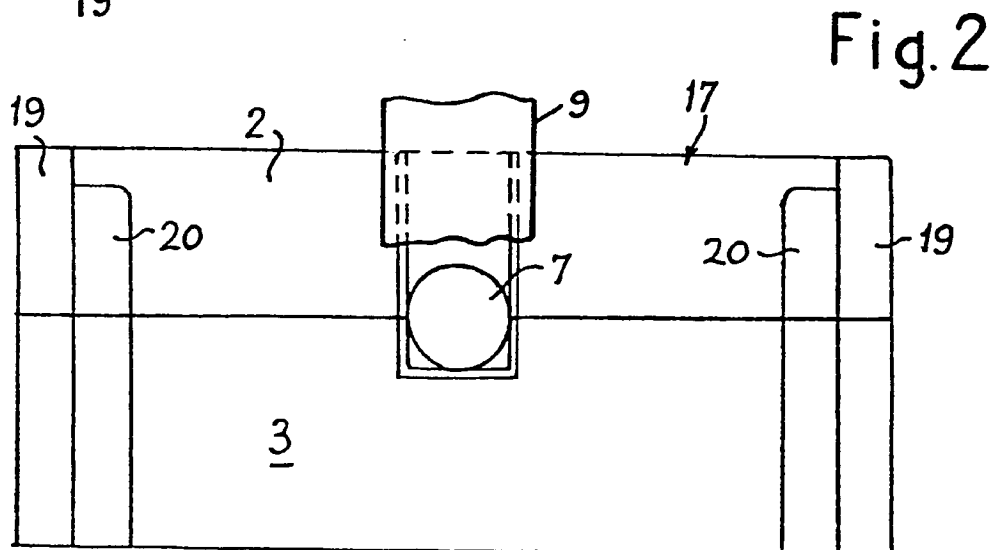
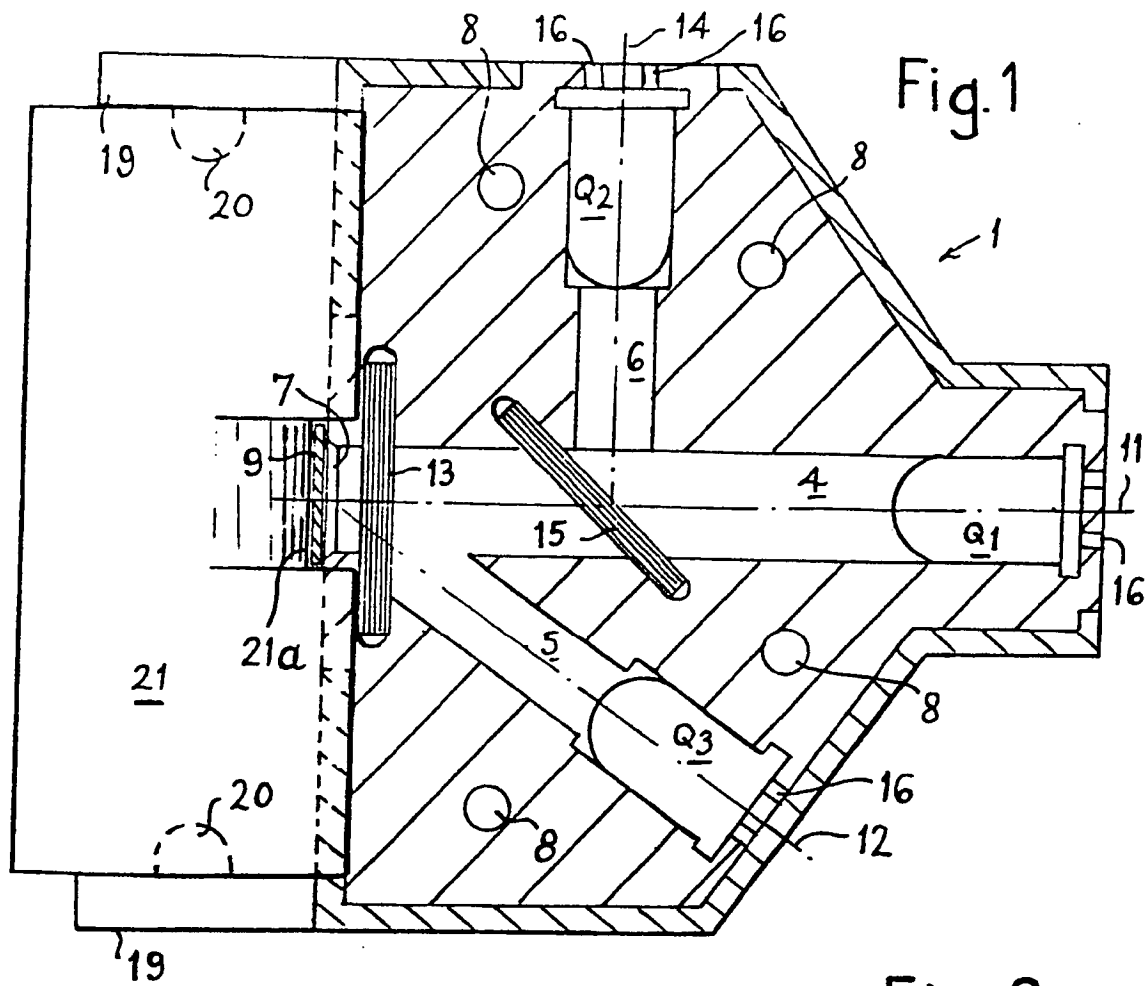
- 1 the reference sensor (Q2) with a reference signal, and
a switching device (Q6) for controlling the light
source (Q1) and which is responsive to the comparator
means, whereby to actuate the light source so as to
5 maintain the control signal generally at a constant
level, for example, the level of the reference signal.
9. A reflectometer according to claim 7 or 8,
characterised by a reference sensor amplifier (U2) for
the reference photosensor (Q2), a first integrating
10 circuit (R12,C14) for integrating the output of said
reference sensor amplifier, and a first voltage divider
(R13-R16) connected to the output of said amplifier,
said control signal for the drive circuit being derived
from said first voltage divider.
- 15 10. A reflectometer according to claim 7, 8 or 9,
characterised by means (25) for producing a digital
reflectance signal corresponding to the reflectance
sensor output.
- 20 11. A reflectometer according to claim 10,
characterised by a reflectance sensor amplifier (U1)
for the reflectance sensor (Q3), a second integrating
circuit (R7,C13) for integrating the output of said
reflectance sensor amplifier, and means (25) for
processing the output signal of said reflectance sensor
25 amplifier to produce a digital reflectance signal.
12. A reflectometer according to claim 10 or 11,
characterised in that the means for producing a digital
reflectance signal includes an analog-to-digital
converter (25) which compares an analog reflectance
30 signal derived from the reflectance sensor output with
a reference signal and produces a pulse train having a
pulse rate corresponding to the analog reflectance
signal.
13. A reflectometer according to claim 12,

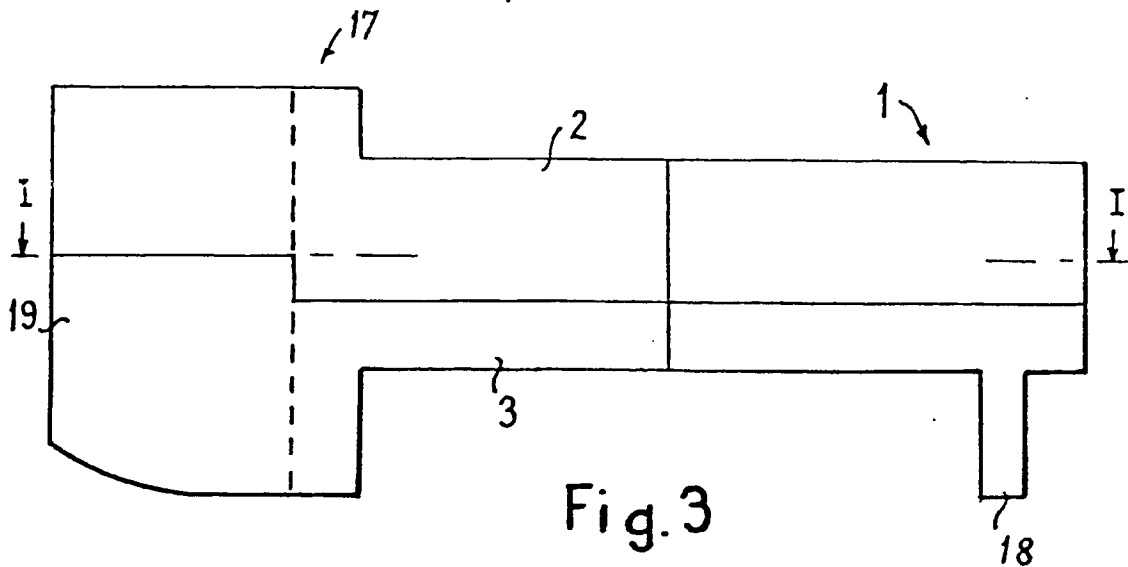
1 characterised by a fixed gain amplifier (U3D) having
inputs connected to the output of the reflectance
sensor amplifier (U1) and the first voltage divider
(R13-R16), respectively, said analog-to-digital
5 converter (25) being connected to the output of the
fixed gain amplifier, and the connection of the drive
circuit to the first voltage divider being adjustable
so as to determine the light standard reflectance and
the connection of the fixed gain amplifier (U3D) to the
10 first voltage divider being adjustable to determine the
dark standard reference.

14. A reflectometer according to claim 12 or 13,
characterised by a second voltage divider (R9,R10) for
producing the reference signal, and a reference
15 amplifier (U3A), said second voltage divider being
connected to the drive circuit and the reference
amplifier, and the output of said reference amplifier
(U3A) being connected to the analog-to-digital
converter (25).

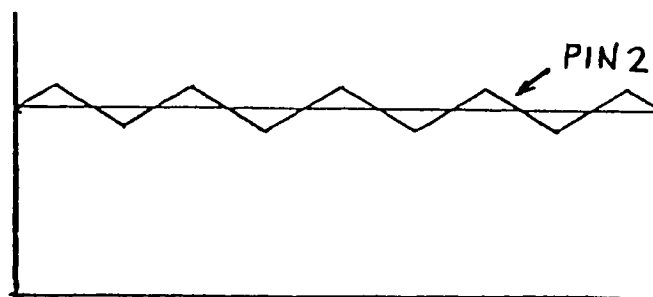
20 15. A reflectometer according to claim 14, wherein the
analog-to-digital converter (25) compares the analog
reflectance signal and the reference signal derived
from the reference amplifier (U3A) and produces a
digital reflectance signal in the form of a pulse train
25 having a pulse rate corresponding to the analog
reflectance signal.

16. A reflectometer according to any preceding claim
10 to 15, characterised by central processing means
(U6) for processing the digital reflectance signal and
30 producing a measurement of reflectance.



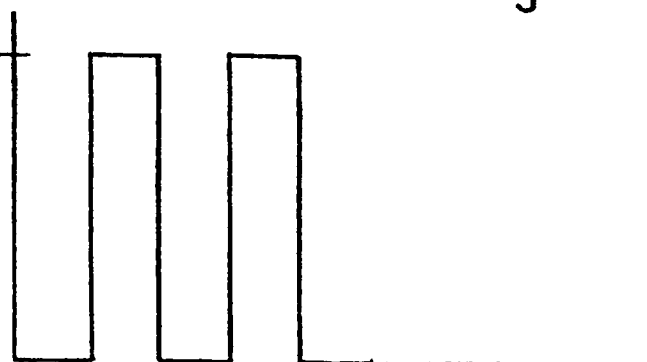


U3B
PINS 3 AND 2
VREF.



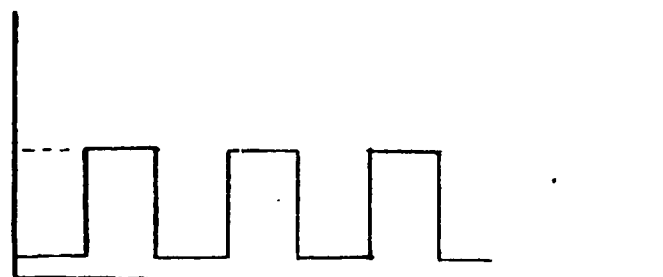
U3B PIN 1
Vcc - 1.5

Fig. 6



Q1 ANODE
1.2 VOLTS

Fig. 7



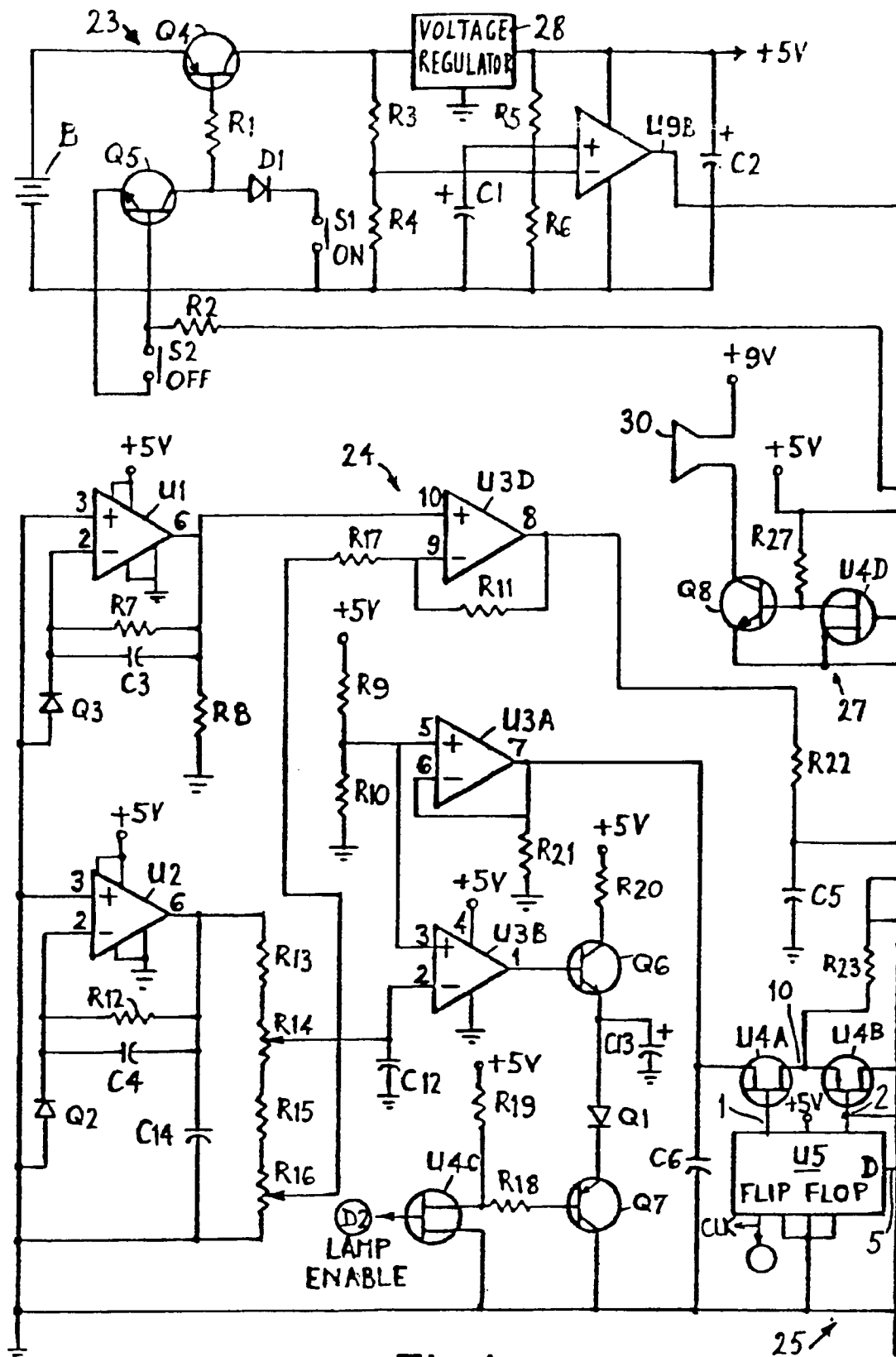


Fig.4

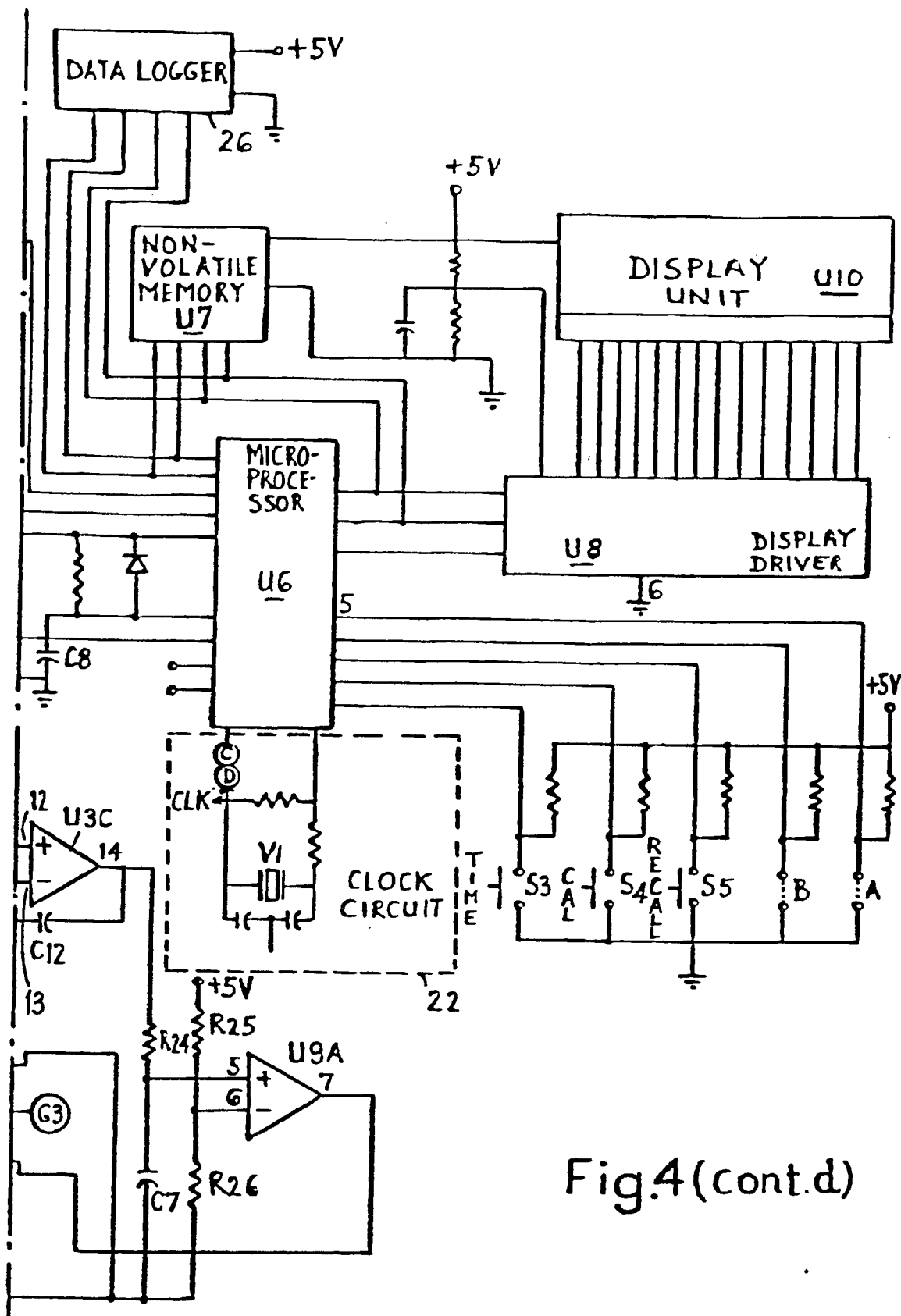


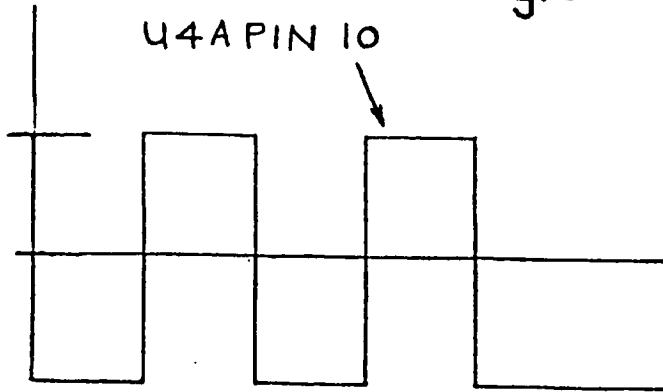
Fig.4(cont.d)

U3C PIN 12 AND 13
ASSUMES $V_{OUT} =$
 $\frac{1}{2} V_{REF}$ V_{REF}

U3D PIN 8 V_{OUT}

U4A PIN 10

Fig.8



U3C PIN 14

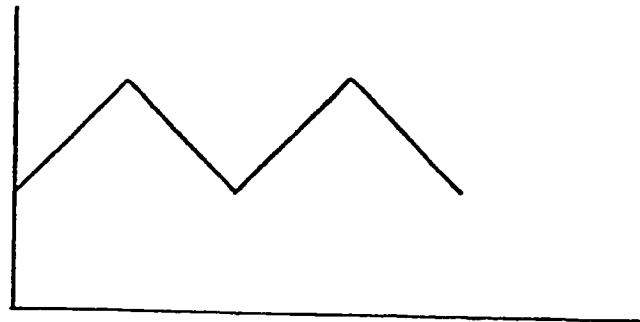
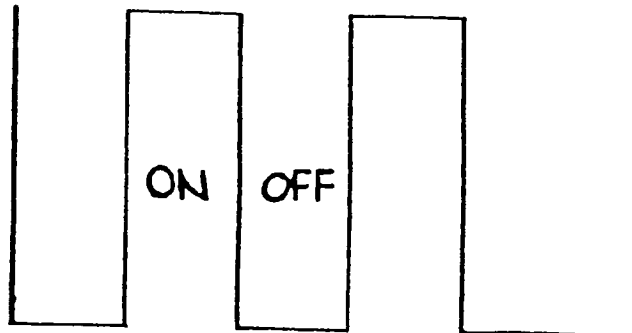


Fig.9

U9A PIN 7 $V_{CC} = 1.5$

Fig.10



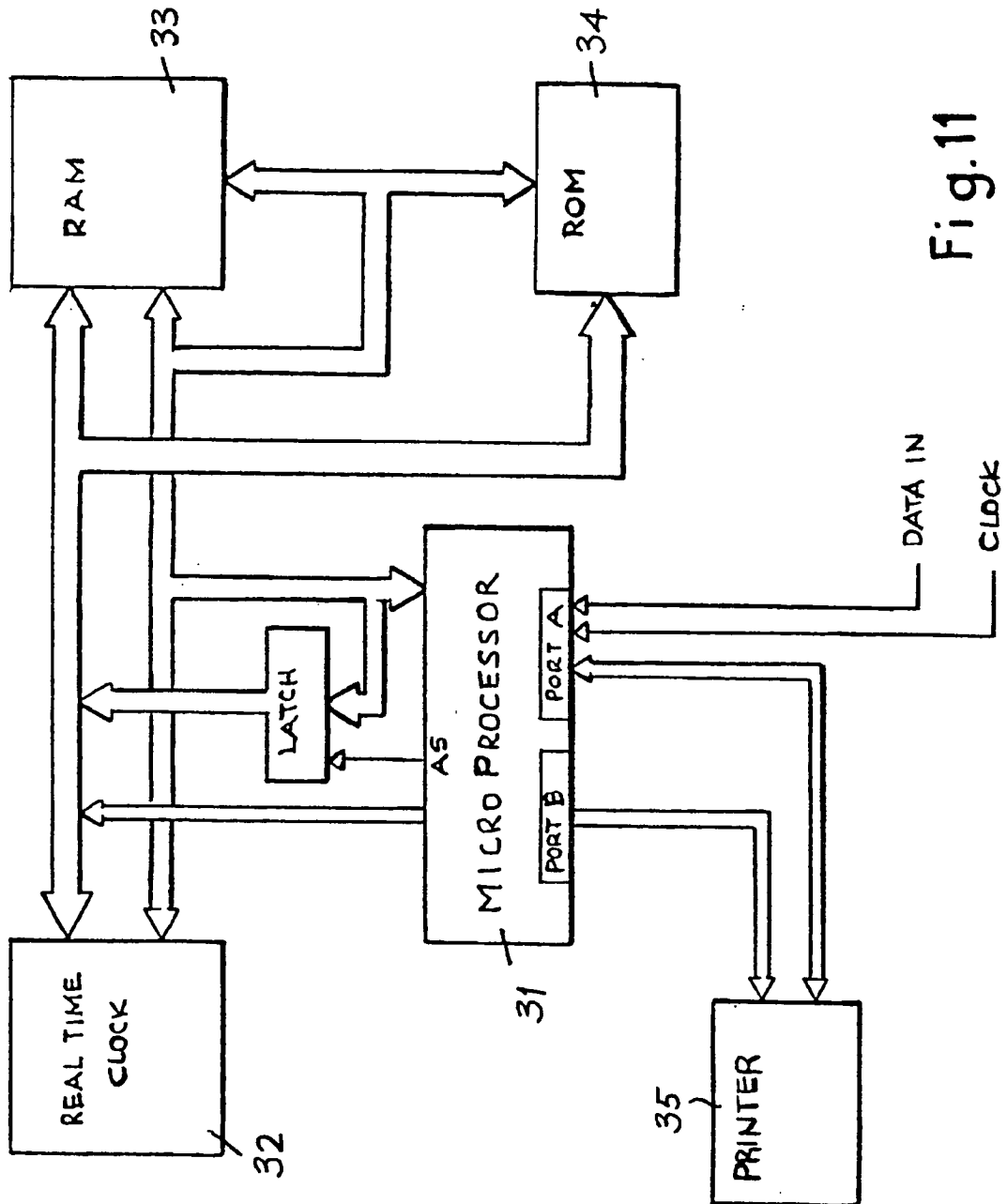


Fig. 11

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